AN MILP Model for Heat Exchanger Networks Retrofit

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This paper addresses the problem of automatically determining the optimal economic retrofit of heat exchanger networks. It is a rigorous MILP (Mixed Integer Linear Programming) approach that considers rearrangement of the existing heat exchanger units, heat transfer area addition and new exchanger installation. We illustrate the method using a crude fractionation unit and we also compare this technique to one existing retrofit approach.

KEYWORDS

Retrofit, Heat Exchanger Networks, Mixed Integer Linear Programming

1. INTRODUCTION

This paper is based on a recently accepted paper for grassroots HEN design. The method consists of a rigorous MILP strategy that is based on a transportation/transshipment strategy. This strategy can handle stream splits and non-isothermal mixing rigorously, without any approximations.

For the case of retrofit, we have added constraints that are able to handle the fact that there is an existing network. The proposed retrofit method as well as the previous HENS design procedure is able to solve complex systems. This is illustrated through 2 application examples.

2. OUTLINE APPROACH FOR RETROFIT

The MILP model is based on the transportation-transshipment paradigm which has the following features:

- Counts heat exchangers units and shells
- Determines the area required for each exchanger unit or shell
- Controls the total number of units
- Determines the flow rates in splits
- Handles non-isothermal mixing
- · Identifies bypasses in split situations when convenient

- Controls the temperature approximation (ΔT_{min}) when desired
- · Can address areas or temperature zones
- Allows multiple matches between two streams

The model considers a consecutive series of heat exchangers. Heat transfer is accounted using the cumulative heat transferred from intervals up to a specific interval to other counterpart intervals. The key of the model and what differentiates it from other transport/transshipment models is the flow rate consistency equations that allow tracking flows in splits. For retrofit situations, the MILP model is extended by adding constraints as follows:

$$A_{ij}^{z} \le A_{ij}^{z^{0}} + \Delta A_{ij}^{z^{0}} + A_{ij}^{z^{N}}$$
⁽¹⁾

$$\Delta A_{ij}^{z^0} \le \Delta A_{ij\,\max}^{z^0} \tag{2}$$

$$U_{ij}^z \le U_{ij\,\max}^z \tag{3}$$

$$A_{ij}^{z^{N}} \le A_{ij\,\max}^{z^{N}} \cdot \left(U_{ij}^{z} - U_{ij}^{z^{0}} \right)$$
(4)

where A_{ij}^{z} is the new area of an exchanger between streams i and j, $A_{ij}^{z^{0}}$ its orinignal area, $\Delta A_{ij}^{z^{0}}$ the additional area to the existing shell, $\Delta A_{ij}^{z^{N}}$ the new area in new shells, and U_{ij}^{z} and $U_{ij}^{z^{0}}$ the new and original number of shells, respectively. Maximum values ($\Delta A_{ij}^{z^{0}}$ and U_{ij}^{z} and U_{ij}^{z} are also used. When original values are zero, then a new match is added.

The objective function for the retrofit heat exchanger network structure is the total annualized cost which consisted of utility cost, additional area cost and fixed cost for new exchanger installation. All terms of the hot and cold utility cost are the same as in the grassroots design model, but the retrofit programming model has complicated functions for the area cost. In the following, the objective function for the proposed retrofit approach is expressed.

$$\begin{aligned} \text{Min } Cost = & \sum_{z \ i \in HU^{z}} \sum_{\substack{j \in C^{z} \\ (i,j) \in P}} c_{i}^{H} F_{i}^{H} \Delta T_{i} + \sum_{z \ j \in CU^{z}} \sum_{\substack{i \in H^{z} \\ (i,j) \in P}} c_{j}^{C} F_{j}^{C} \Delta T_{j} + \sum_{z \ i \in H^{z}} \sum_{\substack{j \in C^{z} \\ (i,j) \in P}} c_{ij}^{F} \left(U_{ij}^{z} - U_{ij}^{z^{0}} \right) \\ & + \sum_{z \ i \in H^{z}} \sum_{\substack{j \in C^{z} \\ (i,j) \in P \\ (i,j) \in B}} \left(c_{ij}^{a^{0}} \Delta A_{ij}^{z^{0}} + c_{ij}^{A^{N}} A_{ij}^{z^{N}} \right) + \sum_{z \ i \in H^{z}} \sum_{\substack{j \in C^{z} \\ z \ i \in H^{z} \\ (i,j) \in B}} \sum_{\substack{k \in H^{z} \\ k = 1 \\ (i,j) \in B}} \sum_{k = 1}^{k} \left(c_{ij}^{a^{0}} \Delta A_{ij}^{z,k^{0}} + c_{ij}^{A^{N}} A_{ij}^{z,k^{N}} \right) \end{aligned}$$

$$(5)$$

Especial constraints are added when more than one exchanger between two streams is allowed. We omit these and concentrate more in showing results.

3. EXAMPLES

In this section, two examples are solved to illustrate the rigorous MILP method. The optimization model was constructed in GAMS and run in a PC with a 2.4 GHz processor and 1 Gb of ram memory.

Example 1

Example 1 is the retrofit problem of crude distillation unit that composed of 18 streams and 18 existing exchangers. Streams properties are shown in Table 1 and Table 2 while the results of retrofit network are given in Table 3 and 4. Cost comparisons are given in Table 5. The retrofit solution achieves 24.06% annual cost savings with two new exchanger units and three shells addition. The original and retrofit networks are shown in Figure 1 and Figure 2.

We report a solution that consumes 9577.781 sec. to reach 0.00% Gap. The original and retrofit networks are shown in Figure 1 and Figure 2. If solution time is an issue one can use several other solutions with smaller gap. One in particular has 20.8% annual cost savings with also two new exchanger units and three new shells that is obtained in 1001.062 seconds.

Stream	F	Ср	Tin	Tout	h
	Ton/hr	KJ/kg-C	С	С	MJ/h-m2
I1	155.1	3.161	319.4	244.1	4.653
I2	5.695	4.325	73.24	30	18.211
I4	151.2	2.93	263.5	180.2	4.894
I7	91.81	2.262	73.24	40	4.605
13	251.2	3.111	347.3	202.7	3.21
		2.573	202.7	45	2.278
15	26.03	3.041	45	203.2	4.674
		2.689	203.2	110	3.952
I6	86.14	2.831	110	147.3	4.835
		2.442	147.3	50	3.8
18	63.99	2.854	50	176	5.023
		2.606	176	120	4.846
19	239.1	2.595	167.1	116.1	4.995
		2.372	116.1	69.55	4.88
I10	133.8	6.074	146.7	126.7	1.807
		4.745	126.7	99.94	3.373
		9.464	99.94	73.24	6.878
J1	519	2.314	30	108.1	1.858
		2.645	108.1	211.3	2.356
		3.34	211.3	232.2	2.212
J2	496.4	3.54	232.2	343.3	2.835
J3	96.87	13.076	226.2	228.7	11.971
		15.808	228.7	231.8	11.075
I11			250	249	21.6
I12			1000	500	0.4
J4			20	25	13.5
J5			124	125	21.6
J6			174	175	21.6

Table 1 Stream properties for Example1

Utilities	Cost \$/(MJ/hr-yr)		
I11	19.75		
I12	37.222		
J4	1.861		
J5	-6.494		
J6	-12.747		
Heat Exchanger Cost	5291.9+77.788A \$/yr		

Table 2 Cost data for Example1

Table 3 Model statistics for Example1

Model Statistics					
Single Variables	3024				
Discrete Variables	459				
Single Equations	5930				
Non Zero Elements	29046				
Time to reach a feasible solution	9577.781 sec				
Optimality Gap	0.00%				



Figure 1 Original HEN for Example 1



Table 4 Resulting of retrofit heat exchanger for Example 1

HE	Original Load	Retrofit Load	Original Area	Retrofit Area	Area Addition	Shell Addition	Cost
	MJ/hr	MJ/hr	m2	m2	m2		\$
1	160,311.20	155,868.90	4,303.20	3,926.25			
2	6,903.09	6,903.09	59.40	63.80	4.40		342.03
3	17,118.40	9,628.07	33.40	21.53			
4	658.00	6,560.99	2.30	16.63	14.33	YES	6,406.84
5	2,554.70	0.02	26.30	28.93	2.63		204.58
6	2,410.70	9,902.58	24.60	398.53	373.93	YES	34,379.01
7	1,065.04	1,065.04	5.50	5.87	0.37		28.70
8	45,024.40	6,042.97	145.00	41.66			
9	100,642.70	63,561.25	1,212.70	962.01			
10	4,473.60	4,045.64	93.70	93.70			
11	54,618.70	59,060.59	685.70	1,239.90	554.20	YES	48,402.09
12	6,293.80	3,373.45	40.00	44.00	4.00		311.15
13	58,044.30	58,042.28	183.30	182.39			
14	36,903.20	36,903.23	101.60	101.47			
15	36,917.40	0	93.90	0			
16	67,053.08	67,053.08	278.10	288.97	10.87		845.32
17	7,913.77	7,913.77	53.50	52.24			
18	136,138.80	95,207.49	976.40	709.00			
19		36,917.41		727.96			61,918.53
20		38,981.58		651.93			56,004.54
			8,318.60	9,556.76	14.88%	3	208,842.80

Table 5 Annual cost comparison between original and retrofit network

Cost	Existing	Retrofit	
\$/yr			
Total utility cost	6,865,616.51	5,004,800.230	
Total fixed and area cost	-	208,842.80	
Totat cost	6,865,616.51	5,213,643.031	
Cost saving		24.06%	

Example 2

We now compare our method with Hypertargets (Briones and Kokossis, 1999). Table 6 shows the stream and cost data for crude distillation unit which consisted of 12 streams and 11 existing units. Figure 3 shows the original network and Figure 4 shows the retrofit structure generated by our MILP strategy. Hypertargets established two retrofit designs (B1 and B2) with the same utility cost and one new unit in each case. They are shown in Figure 5 and 6. Our MILP approach suggests using two new smaller exchangers and more utility. The results are shown in Tables 7 and 8 and the total annual cost in Table 9. The retrofit has a 4.17% saving over the original structure.

Table 6 Stream and cost data for Example 2

Stream	FCp	Tin	Tout	h
	kW/C	С	С	kW/m2-C
I1	470.00	140.00	40.00	0.8
I2	825.00	160.00	120.00	0.8
I3	42.42	210.00	45.00	0.8
I4	100.00	260.00	60.00	0.8
I5	357.14	280.00	210.00	0.8
I6	50.00	350.00	170.00	0.8
I7	136.36	380.00	160.00	0.8
J1	826.09	270.00	385.00	0.8
J2	500.00	130.00	270.00	0.8
J3	363.64	20.00	130.00	0.8
18		500.00	499.00	0.8
J4		20.00	40.00	0.8

Note: Exchanger cost=300xArea; stream cost=60\$/kW yr; cooling water cost=5\$/kW yr



Figure 3 Original HEN for Example 2



Figure 5 Hypertarget retrofit designs B1

Table 7 Model statistics for Example 2

Model Statistics						
Single Variables	3120					
Discrete Variables	382					
Single Equations	6347					
Non Zero Elements	23949					
Time to reach a feasible solution	411.41 sec					
Optimality Gap	0.00%					



Figure 4 Retrofit HEN for Example 2



Figure 6 Hypertarget retrofit designs B2

HE	Original Load	Retrofit Load	Original Area	Retrofit Area	Area addition	Shell Addition	Cost
	MJ/hr	MJ/hr	m2	m2	m2		\$
1	47,000.00	47,000.00	2,363.86	2,402.06	38.198		
2	33,000.00	33,000.00	1,609.62	1,613.93	4.310	YES	1,293.106
3	7,000.00	7,000.00	230.69	242.32	11.628	YES	3,488.465
4	10,200.00	8,711.41	692.14	692.14			
5	9,800.00	11,287.49	339.80	366.26	26.457		
6	25,000.00	25,000.00	1,226.76	1,286.34	59.581	YES	17,874.203
7	9,000.00	9,000.00	224.92	396.58	171.669	YES	51,500.690
8	20,800.00	20,813.59	1,211.00	1,211.00			
9	9,200.00	1,127.37	141.47	20.48			
10	95,000.00	86,942.11	1,434.98	1,344.35			
11	5,000.00	6,475.20	53.31	66.93	13.617		
12		1.10		0.05	NEW		15.300
13		8,058.24		298.33	NEW		89,499.000
			9,528.54	9,940.77	4.33%	4	163,670.763

Table 8 Resulting of retrofit heat exchanger network for Example2

Table 9 Annual cost comparison between Hypertargets and MILP algorithm

Cost	Existing	Hypertarget B1	Hypertarget B2	MILP
	\$/yr	\$/yr	\$/yr	\$/yr
Total utility cost	6,330,000	5,607,200	5,607,200	5,902,113
Total fixed and area cost		531,900	576,720	163,671
Totat cost	6,330,000	6,139,100	6,183,920	6,065,784
MILP more saving (\$/yr)	264,216	73,316	118,136	
	4.17%	1.19%	1.91%	

4. CONCLUSION

A new MILP formulation for the retrofit of heat exchanger networks, which takes into account the retrofit options involving modification of the existing structure and new exchanger placement, was presented. The model is very robust and capable of handling *rigorously* large networks such as those of crude distillation units.

5. REFERENCES

- Barbaro A. and M. Bagajewicz, New Rigorous One-step MILP Formulation for Heat Exchanger Network Synthesis. Computers and Chemical Engineering. Submitted. (available at http://www.ou.edu/class/che-design/unpubpapers/HEN-MILP.pdf) Jan 2004
- V. Briones and A.C. Kokossis, 1999, Hypertargets: a Conceptual Programming Approach for the Optimisation of Industrial Heat Exchanger Networks-II. Retrofit Design. Chem.Eng.Sci, 54, 541-561.