

# (IX) EXERCISES ON ADVANCED PROCESS DYNAMICS AND CONTROL

by

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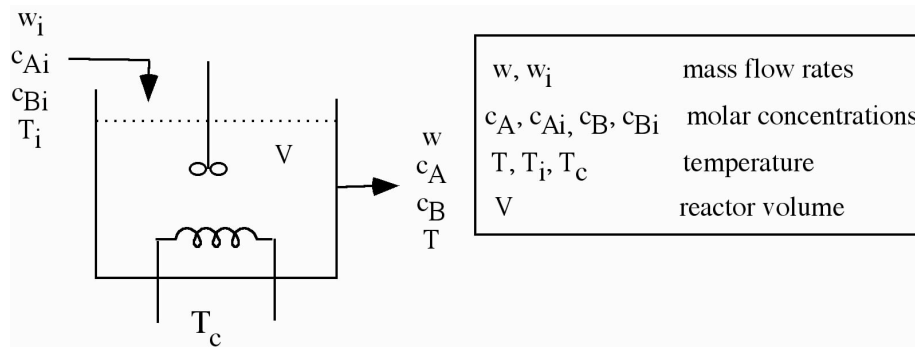
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## Exercise 1

- (Problem adapted from problem 4.13 of the textbook by Seborg, Edgar, and Mellichamp)
  - Derive a nonlinear dynamic model for the reacting system shown in the figure below



- Irreversible chemical reaction
  - $2A \rightarrow 2B$ .
  - Exothermic with heat of reaction  $(-\Delta H_{rxn})$ .
  - Rate of reaction of species A is  $r_A = -k C$ ,  $k = k_o \exp(-E/RT)$
  
- Cooling coil
  - Heat transfer area  $A_c$
  - Liquid coolant stays at temperature  $T_c$
  
- The inlet and outlet mass flow rates may vary with time, depending on upstream and downstream process conditions

## Exercise 2

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- Consider the matrix  $A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}$ 
  - (1) Derive an expression for  $\det(sI - A)$
  - (2) Find the eigenvalues and state their **algebraic** multiplicity
  - (3) Find the eigenvalues and state their **algebraic** multiplicity
  - (4) Find a set of **linearly dependent** eigenvectors
  - (5) Find a set of **linearly independent** eigenvectors
  - (6) State the **geometric** multiplicity of the eigenvalues
  - (7) Calculate the matrix exponential function  $e^{At}$

## Exercise 3

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- Consider the LTI system

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 2 & 0 \\ -2 & -20 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$

with initial conditions

$$\begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 10 \\ 6 \end{bmatrix}$$

- Calculate the response of the system to the constant-forcing input

$$\begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix} = \begin{bmatrix} 0.5 \\ 0.1 \end{bmatrix}$$

## Exercise 4

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- Consider the LTI system

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 2 & 0 \\ -2 & -20 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$

with initial conditions

$$\begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 10 \\ 6 \end{bmatrix}$$

- Is the system controllable?
- Is the homogeneous state-space stable with respect to the initial conditions?
- Is the zero-input system BIBO stable?

# Exercise 5

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- Consider the LTI system

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 2 & 0 \\ -2 & -20 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$

with initial conditions

$$\begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 10 \\ 6 \end{bmatrix}$$

- Design a state-feedback control law

$$\mathbf{u}(t) = -\mathbf{K} \mathbf{x}(t)$$

that places the eigenvalues of the closed-loop system at the locations

$$\{-2, -4\}$$

- *Hint 1:* Note that the system is controllable when the input matrix is  $\mathbf{B} = \begin{bmatrix} 2 & 0 \\ -2 & -20 \end{bmatrix} = [\mathbf{b}_1 \ \mathbf{b}_2]$ , and when the input matrix is  $\mathbf{B} = \mathbf{b}_1$ . On the other hand, the system is not controllable with respect to the input matrix  $\mathbf{B} = \mathbf{b}_2$

- *Hint 2.* Use Ackermann's formula for input  $u_1(t)$  to find a gain

$$\mathbf{k}^T = [k_1 \ k_2], \text{ and then define } \mathbf{K} = \begin{bmatrix} k_1 & k_2 \\ 0 & 0 \end{bmatrix}$$

- *Question:* why would the approach of *Hint 2* fail if one were to use input  $u_2(t)$  instead of  $u_1(t)$ ?

# Exercise 6

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- Consider the LTI system

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 2 & 0 \\ -2 & -20 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$

with initial conditions

$$\begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 10 \\ 6 \end{bmatrix}$$

- Design a state-feedback tracking controller

$$\mathbf{u}(t) = -\mathbf{K} \mathbf{x}(t) - \mathbf{K}_r \mathbf{r}(t)$$

that ensures zero offset for all set points  $\mathbf{r}(t)$  that have a constant final value.